

Amendments to the Specification:

Please replace the Specification of the present application, including the Abstract, with the following Substitute Specification. A marked-up version of the Substitute Specification and Abstract is attached hereto.

SPECIFICATION

TITLE OF THE INVENTION

LINEAR AMPLIFIER ARRANGEMENT WITH NON-LINEAR AMPLIFIER
ELEMENT FOR A MOBILE RADIO DEVICE

FIELD OF TECHNOLOGY

[0001] The present disclosure relates to a method and a device for optimizing the efficiency of an amplifier arrangement with a non-linear power amplifier, preferably in a mobile radio device.

BACKGROUND

[0002] As part of the further development of mobile radio from the GSM standard to EDGE or further on to the UMTS standard, new demands are being made on the transmission characteristics of power amplifiers. Previously, information was transmitted as pure phase information (GMSK), however, recent developments require that the amplitude be also evaluated for information transmission. This results in more stringent requirements for the transmission characteristics of power amplifiers. On the one hand the amplifier element must be linear, and on the other hand the transmission characteristics must not depend on temperature changes and operating voltage variations. However, this is not always the case using transistors. Often times linear and non-linear distortions need to be minimized. To achieve this, a pre-equalization in the base band or intermediate frequency or in the form of a closed loop such as a polar loop is implemented. However, in each case a significant balancing and/or circuit overhead is required with such an arrangement.

[0003] Accordingly, an efficient and cost-effective amplifier arrangement is needed.

BRIEF SUMMARY

[0004] The present disclosure illustrates an amplifier arrangement having a non-linear power amplifier (LV) and two successive push-pull phase modifiers (PS), where a signal offset in phase to the input signal is generated in each case. Afterwards, the phase modifiers power dissipation is converted at a passive

component. The passive component is connected to the outputs of the phase modifiers. A passive component can, for example, be a load balancing resistor or a symmetrical transformer with a subsequent rectifier arrangement. After the power amplifier, the amplitude-modulated signal is divided up into two signal parts of equal size or part powers and routed via two push-pull phase modifiers. The use of a symmetrical transformer as the component is particularly advantageous. The voltage uncoupled in the symmetrical transformer in this case is forwarded to a rectifier and the direct current output by the rectifier is routed to a supply unit as charge current. One advantage of this amplifier arrangement is that the efficiency of this arrangement can be decisively improved. Furthermore, the present method and arrangement of very cost effective.

BRIEF DESCRIPTION OF THE DRAWINGS

[0005] The various objects, advantages and novel features of the present disclosure will be more readily apprehended from the following Detailed Description when read in conjunction with the enclosed drawings, in which:

[0006] Figure 1 illustrates a power amplifier with subsequent modulation feed and load balancing resistor, and

[0007] Figure 2 illustrates an amplifier arrangement for feeding back electrical energy to a supply unit of a mobile radio device.

DETAILED DESCRIPTION

[0008] Figure 1 shows an amplifier arrangement for implementing a linear amplifier system with non-linear amplifier components. Two phase modifiers PS controllable with a modulation signal are connected after a C-class power amplifier LV (where efficiency can be realized in practice in the range of 75%). The circuit of Figure 1 can be implemented with any class of amplifier (A, B or CC). However, the efficiency may be degraded with an amplifier LV operated other than in C class mode.

[0009] After the power amplifier LV, the generated signal or the power PRF is divided up into two part signals or part powers of equal size PRF 1 and PRF 2. These part powers are routed via the push-pull phase modifiers PS. In accordance with amplitude information, the power (RF) is converted as power

dissipation in the load balancing resistor LAW. Amplitude information in this case is envelope curve information. The main disadvantage of this circuit arrangement also arises here. Corresponding to the crest factor (ratio of peak power to average power) the C-class power amplifier LV must be arranged for the peak power to be transmitted. However in such a circuit arrangement this leads to a large part of the RF power generated PRF being converted in the load balancing resistor LAW.

[0010] Figure 2 shows a amplifier arrangement for feeding back electrical energy to a supply unit of a mobile radio device. The power amplifier LV from Figure 1 can again be seen in this diagram operating in C-class mode with subsequent power separation PRF 1 and PRF 2 and the controllable phase modifiers PS. The circuit of Figure 2 works with any class of amplifier (A, B or C), however the efficiency may be degraded with a power amplifier LV operated other than in C mode. Omitted from this diagram is the load balancing resistor LAW which is replaced by a symmetrical transformer SÜ (ballun). Furthermore, a rectifier arrangement GR connected to a direct current supply unit VE is added. The task of this new circuit arrangement is to route the dissipated power (HF) of the power supply unit (battery, ac adapter etc.) previously converted in the load balancing resistor LAW to a mobile radio device, and a mobile station for a cellular mobile radio network, as direct current. After the power amplifier LV, power components PRF 1 and PRF 2 are routed via the phase modifiers PS. The electrical length or the throughput time of the power components PRF 1 and PRF 2 is influenced with phase modifiers PS. Thus, as an example, power component PRF 1 is increased in path 1 by phase modifier PS, and the delay time in path 2 is reduced by the other phase modifier PS (push-pull). This is achieved through two vectors which have the same phase angle before the phase modifier PS and are different after the phase modifier PS. This produces a different length of sum vector for the addition of the two subvectors before and after the phase modifiers PS as regards the amount. The phase modifiers PS are controlled by an amplitude modulation signal, which, for example, can be an audio signal, video signal or similar information. The amplitude modulation signal can be decoupled from the input signal (useful signal). However it can also be any given signal. If the control voltage of the phase modifiers PS is

not equal to zero, there is a voltage drop at the symmetrical transformer SÜ. The control voltage corresponds to the amplitude modulation signal and is thus zero when the modulation voltage is zero, via the symmetrical amplifier SU this voltage is transmitted on the secondary side of the transformer SÜ and referenced there to a potential. In this example, this is represented by a ground symbol. A reference to a battery potential, for example, is however also always conceivable. Subsequently, the voltage is rectified with a multipath rectifier and filtering is performed. The greatest efficiency is preferably obtained with a multipath rectifier. It would also be possible to use another rectifier. The direct current set can then be fed to the supply unit VE. To optimize the functionality of the overall circuit the input impedance of the rectifier GR should be almost independent of amplitude. If the input impedance of the rectifier is not constant, non-linear distortions are created which affect the function of the overall circuit. To transmit all signal components free of distortion, the C amplifier LV is designed for transmitting the maximum peak power occurring in the circuit. This means that the amplifier LV runs with a constant power which lies above the average power required at the output by the crest factor. With normal transmission procedures, the crest factor lies in the range 3dB to 10dB. If the amplifier LV is dimensioned for a crest factor of 10dB, this means that for the arrangement with a load balancing resistor LAW (Figure 1), appr. 90 % of the generated power would be converted in the load balancing resistor LAW as power dissipation. With the expanded circuit there is now the opportunity of capturing a this power dissipation component (HF) and feeding it to a supply unit VE as charge current. An HF (power dissipation) - DC (direct current) conversion is thus performed.

[0011] The above described description and drawings are only to be considered illustrative of exemplary embodiments, which achieve the features and advantages of the invention. Modifications and substitutions to specific process conditions and structures can be made without departing from the spirit and scope of the invention. Accordingly, the invention is not to be considered as being limited by the foregoing description and drawings, but is only limited by the scope of the appended claims.